## Designer's casebook

## Voltage-controlled integrator sets filter's bandwidth

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Because it uses operational transconductance amplifiers as electrically tuned integrators for selecting a statevariable filter's center frequency and bandwidth virtually independently of one another, this circuit is ideal for use in music and speech synthesizers that require individual voltage-controlled setting of these parameters.

As shown, input signals to be processed are applied to transconductance amplifier A1, whose bias current is derived from voltage-to-current driver  $A_5Q_5$ . The bias current, in turn, is set by control voltage V, which ultimately determines the filter's center frequency. In general,  $I_{bias} = V_{\omega}/2R_{11}$ .

Placing the capacitor C<sub>w</sub> across the output of the operational transconductance amplifiers A1 and A2 converts the two-stage network into a noninverting integra-

tor, the transfer function becoming  $V_o(s)/V_i(s) = k/s$ , where k is the 3080's transconductance factor k'/C, and transconductance k' as given in its data sheets is k' = 19.2  $I_{bias}$ . Substituting for  $I_{bias}$ ,  $V_o(s)/V_i(s) = 19.2$ 

Placing integrator A<sub>3</sub> in the feedback loop of A<sub>1</sub> and A<sub>2</sub> equips the basic filter with the capability to control bandwidth. As seen from inspection of the circuit:

$$V_x(s) = R_1 ||R_2||R_3||R_4 \left[ \frac{V_1(s)}{R_1} + \frac{V_y(s)}{R_3} + \frac{V_{LP}(s)}{R_4} \right]$$

where the low-pass function is given by:

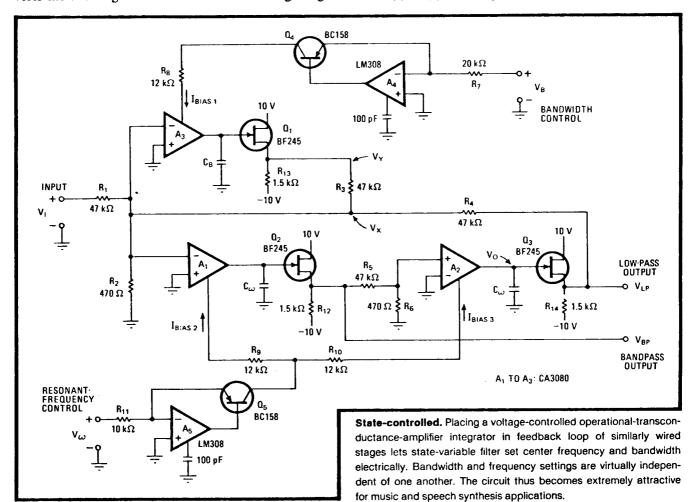
 $V_{LP}(s) = -(k_2/s)^2 V_x(s) R_6/(R_5 + R_6)$ and where  $V_y(s) = -k_1V_x(s)/s$ . Constants  $k_1$  and  $k_2$  are

 $k_1 = 19.2 V_B/R_7 C_B$   $k_2 = 19.2 V_{\omega}/2R_{11} C_{\omega}$ 

and the bandpass function,  $V_{BP}(s)$ , equals  $-k_2V_x(s)/s$ .

Assuming  $R_1 = R_3 = R_4 = R_5 = R'$  and  $R_2 = R_6 = R''$ , with R''/R' = a <<1, it follows that  $R_1 | R_2 | R_3 | R_4 = R_2$ . Substituting the appropriate quantities back into all the above equations, it is seen that:

$$V_{LP}(s)/V_i(s) = -1/[(s/\omega_o)^2 + (B/\omega_o)(s/\omega_o) + 1]$$



VBe(S)/V;(S) = -(S/wo)/[(S/wo)2+(B/Wo)(S/wo)+1] Where the resonant frequency and the bandwidth Electronics/July 31, 1980 are given by: Wo (rad/s) = a k2 = 19, 2 a V/2 RII Compromise Parameter a Sould be near 0,01 to ensure the best compromise